#  <br> Simplified Selection and Application 

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The purpose of this manual is to give you information needed to select the correct pump for the job in simple terms.

This manual contains:

Types of pumps in use today Pages 1-4
How to read a pump performance curve
Pages 5-6
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Pages 7-8
How to select the correct pump for the job
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Useful information
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Page 15

## Types of Pumps in Use Today

## STANDARD CENTRIFUGAL PUMPS

The simplest of all types, it has been in use since the 1700 's. This pump operates on the centrifugal force principle, which can be seen in operation every time you drive your car on a wet road. The tire picks up water and throws it by centrifugal force against the fender.


A centrifugal pump operates on the same principle except the tire is called an impeller and it has blades to move the water.


However, we can't have water going in all directions at once, so we direct it by means of a casing, or volute (pronounced va-loot) as it is called in the pump industry. The volute acts in the same manner as your car fender; it controls the water after it leaves the impeller.

This AMT high head centrifugal pump is ideal for chemical processing, liquid transfer, heating and cooling and sprinkler/fire protection systems.


## SELF-PRIMING PUMPS

This type of pump does a good job as long as the supply of liquid flows to the pump. Put the "Standard Centrifugal Pump" above the liquid, and problems can arise, as it does not have the ability to create a vacuum and prime itself. Should it pump the hole dry and air enter the pump, it will stop pumping and become airbound.


Accessory equipment must be used to evacuate entrained air within the pump, such as an eductor, a hand primer, etc. On construction jobs there is a need for a pump which has the ability to prime itself repeatedly, since the purpose of the pump is to keep the hole dry. As a result, the pump must lower the water below the strainer inlet time and time again, handling large amounts of air at the same time. A pump capable of repriming is a must.

## Types of Pumps in Use Today

Here is how it works:
During the priming cycle, air enters the pump and mixes with water at the impeller. Water and air are discharged together by centrifugal action of the impeller into the water reservoir.

Once in the reservoir, the air and water mixture slows down from its former velocity, allowing air to escape out the discharge. Air-free water, now heavier than airladen water, flows by gravity back down into the impeller chamber, ready to mix with more air coming in the suction line.

Once all air has been evacuated and a vacuum created in the suction line, atmospheric pressure forces water up into the suction line to the impeller, and pumping begins.

Recirculation of water within the pump stops when pumping begins.


This type of pump differs from a standard centrifugal pump in that it has a water reservoir built into the unit which enables it to rid pump and suction line of air by recirculating water within the pump on priming cycle. This water reservoir may be above the impeller.


Or, it may be located in front of the impeller.


This portable IPT model is an example of a self-priming pump.

## Types of Pumps in Use Today

Centrifugal pumps may be manufactured in many different sizes and shapes. Impeller diameter controls the head or pressure; impeller blade controls the flow rate.

Depending upon its intended use, an impeller may have two, three, or even six blades attached. As a rule, impellers designed to handle trashy water will have fewer blades with maximum width. Impellers for highhead or pressure will have more blades of narrow width and may be enclosed on both sides of the blades.

## DIAPHRAGM PUMPS

A diaphragm pump is a plunger-type of pump, similar in operation to the fuel pump in your car.

Figure 1

plunger (fig. 2) - which
moves up and down.

There are check valves on either side of the pump.

On the down stroke, discharge opens and water flows out.
It has a diaphragm
(fig. 1) attached to a

On the up stroke, the suction valve opens and water flows in.

The first practical lightweight diaphragm pump was designed in 1953 - a pump which cut 200 lbs . from the weight and gave up to $400 \%$ more gallons per minute than pumps then available. In addition to using aluminum in major pump parts, a spring was added to the plunger rod to absorb the first shock as the plunger started its down stroke. Result: a smoother running unit and improved diaphragm life. It was extended even longer with material innovations for diaphragms.


Figure 3

Next, a suction accumulator (fig. 3) was placed just ahead of the pump. During up stroke, water is drawn from the accumulator directly into the pump body. During down stroke, when water is being pushed out of the body, the accumulator refills with water, making it available for the next stroke. Result: greatly increased capacity and a smoother running unit.

The combination of the spring and accumulator makes this diaphragm pump the best on the market.

## Types of Pumps in Use Today

## POSITIVE DISPLACEMENT PUMPS

The flow rate of a centrifugal pump will vary with a change in discharge pressure whereas the flow rate of a positive displacement pump will remain relatively constant at variable discharge pressures.

These types of pumps are mostly used where high pressure and low volume are required. They normally will not hold up when pumping dirty water or abrasive liquids, so are not suitable in construction-type pumping applications.

Positive Displacement
 models, such as this G-R heavy-duty rotary gear pump, are versatile enough to handle a wide variety of pumping applications.

## SUBMERSIBLE PUMPS

A standard centrifugal pump, usually driven by an electric motor, both of which are encased in a common housing which can be immersed in water. Submersible pumps do not require priming, as water flows to the pump.

Submersible pumps, such as this slimline model, are ideal for high-head, highvolume applications.


## How To Read Pump Performance Curves

Each pump hasa peffomance curve. These graphs give the actual perfomance of a pump underdifferent sets of conditions. Please see "Curve A" on the next page.

## Cunve "A"

This is a typical curve used to portray performance of the Model 3G5 pump powered by a Briggs \& Stratton 5 HP engine. Note, along the bottom is the capacity in U.S. Gallons per Minute. Along the left edge, amount of pressure the pump will develop is expressed in both pounds pressure and feet. These show the total head the pump will develop. Normally, the "feet" scale is used in figuring a contractor's pump job.

Also on the curve are more lines. A solid line gives the performance of a unit at continuous duty (governed speed) operating conditions such as you would expect on a construction job. Lines marked $25^{\prime}, 20^{\prime}, 15^{\prime}$, and $5^{\prime}$ show maximum gallons per minute the pump is capable of delivering at various suction lifts (height of pump above water).

To read the curve, you may start at either left scale or bottom scale. Let's assume you desire to pump 100 GPM. Follow across the bottom GPM scale until you reach 100; then follow this line until you cross a heavy black line; then straight back to the left to the "feet" scale. What does this tell you? Simply this: the pump is capable of pumping 100 GPM against a total head of approximately 68 feet, provided the pump is no more than 25 feet above water.

Let us say total head is 60 feet. Start at the left on the "feet" scale, at the 60' mark, until a heavy black line is reached; then straight down to the GPM scale. Result: against a total head of 60 feet, the pump will deliver 150 GPM, provided the unit is no more than 20 feet above water. If the unit is 25 feet above water, the most you could expect would be about 125 GPM.

Curve "A"



Curve "B"
Many times your customer will desire to use an electric motor driven pump. Curves depicting performance of these pumps are slightly different. Curve "B" illustrates these differences, for the same pump model as Curve "A"

## Curve "B"

There are more lines on this curve than on gasoline engine-driven pump curves. These extra lines are (1) RPM (Revolutions Per Minute), which illustrates performance at various speeds; (2) horsepower at various RPMs is also indicated and on Curve " B " is marked 1 to 6 BHP. This information is needed to pick the right size motor; (3) there is a chart which shows the maximum vertical distance that the pump will prime at various speeds marked maximum priming; (4) then there are lines marked static lift. Use these lines to determine a pump's suction lift The result is maximum suction lift at which pump can be placed and still deliver desired gallons per minute.

Example: To pump 220 GPM, pump must be within 15 feet of water. Simple, isn't it? If you are operating a pump at higher elevations of 2,000' to 5,000' above sea level, refer to Page 9 for altitude deduction which must be taken into account.

An important item to remember in use of electric motor-driven pumps is the fact motors operate at a
constant speed. Their RPM cannot be varied as can most gasoline or diesel engines.

Electric Motor Speeds (RPM)

## 60 Cycle

3450 1750 1150

50 Cycle
2950
1450
850

## 25 Cycle

1450
725
450

60 Cycle is the most prevalent in North America, with 50 Cycle the most common elsewhere.

Using Model 3G5P pump as an example, we could not expect this pump directly connected to a 3500 RPM motor to deliver as much as engine driven model 3G5, which operates at a higher speed.

To select the proper size motor, it is only necessary to refer to the RPM line at which pump is to be driven. Operation at 2900 RPM requires a 3 HP motor, as shown on the curve; and for operation at 3500 RPM, a 5 HP , 3450 RPM motor is needed. Note: 3500 RPM line starts at 3 HP and goes up to 5 HP . This means you would overload a 3 HP motor, as it is necessary to use 5 HP .

## Understanding Pump Applications

Let us assume a contractor estimates water flow in a ditch he is digging at 200 GPM (gallons per minute). [See Table 2, page 13] The ditch is 5 feet deep and we must push water over an embankment 10 feet high and 80 feet away.

The contractor has estimated 200 GPM, but we know from past experience that not every person is a good judge of water flow and the contractor may run
into additional water. So , to be on the safe side, we assume his maximum water requirement may be 225 GPM.

From the picture below, we see our customer has a suction lift (height of pump above the water) of 5 feet. He also has a discharge head (how high the water must be pushed vertically) of 10 feet.


Next we must figure friction loss in total length of hose, piping and fittings:

1) Suction hose
2) Strainer loss (equals 5 feet of pipe)
3) Discharge piping
4) $1-90 \cong$ elbow ( $=8$ feet of pipe)

Total length of pipe, hose, fittings

| Check with |
| :---: |
| Table |
| $10^{\prime}$ |
| $5^{\prime}$ |
| $100^{\prime}$ |
| $8^{\prime}$ |
| $123^{\prime}$ |

Next, we refer to Page 10 of this book for the friction loss table. Here we find it is impractical to use smaller than $3^{\prime \prime}$ pipe or hose for 225 GPM. We note friction loss for 250 GPM through $3^{\prime \prime}$ pipe is 14.8 feet per 100 feet of hose. Since we have a total of 123 feet, we multiply 1.23 times 14.8 and find our total loss in hose is 18.2 feet.

We then add together the following:

Suction lift
Discharge head 5'

Friction loss in hose
Total head, including friction loss
(Known as TDH, Total Dynamic Head)

We must now find a pump which will give us 225 gallons per minute at a total head of 33.2 feet with the pump 10 feet above water.

## Understanding Pump Applications



Here we note our head condition of 33.2 feet is close to curve of the 3G5, at which point the pump will
deliver 240 GPM when 10 feet above water. Therefore, we select a 3 inch pump.

## How to Select the Right Pump for the Job

Nine times out of ten, your customer will tell you he wants a 2-, 3- or 4 -inch pump. Sometimes, however, your customer will ask you to figure the correct pump for a certain application. There are several things we must know before we attempt to select the proper pump:

1) How many gallons per minute are we going to pump?
2) How high is the pump above water?
3) How high must the water be pushed after it leaves the pump?
4) The total length of hose or pipe to be used.
5) Is water merely to be "dumped" at the end of the discharge run, or will it be used to perform work? (See Special Conditions in Figuring Pump Applications)

## How to Select the Right Pump for the Job SPECIAL CONDITIONS IN FIGURING PUMP APPLICATIONS

## PRESSURE REQUIRED AT END OF DISCHARGE LINE

Some applications, such as gravel washing, jetting, piling, and borrow pit sprinkling, require not only delivering water at a point some distance from the pump, but also supplying a certain amount of pressure at the end of the line. As an example, if 40 pounds of pressure were required for gravel washing in our illustration, this figure must be added to the result of our first four steps. It is easier to convert pounds pressure to feet of head, as we have used feet in figuring the application. From the table on Page 14 you will note 40 pounds is equal to approximately 92.3 feet of head. Here is the result:

Total Head, including friction loss
Pressure required at end of pipe
51.2'

New Total Head (TDH)
92.3'
143.5'

We now need to make a new pump selection.

| To Convert | Inтo | Multply By |
| :--- | :---: | ---: |
| Pounds per sq. in. | Feet of Water | 2.31 |
| Feet (of water) | Pounds per sq. in. | .433 |
| Inches of Mercury | Feet of Water | 1.133 |
|  | (also see Pagel2) |  |

## APPLICATIONS AT <br> HIGHER ELEVATIONS

Pump performance is calculated and plotted on all published data at sea level. At elevations of 1,000 feet and below, this data may generally safely be used, but at higher elevations both pump and engine lose output.

Following is listed the loss in performance which may be expected compared with sea level performance:

| Elevation | GPM | Head |
| :---: | :---: | :---: |
| 2,000 Feet | $-3 \%$ | $-5 \%$ |
| 4,000 Feet | $-5 \%$ | $-9 \%$ |
| 6,000 Feet | $-7 \%$ | $-13 \%$ |
| 8,000 Feet | $-9 \%$ | $-17 \%$ |
| 10,000 Feet | $-12 \%$ | $-22 \%$ |

Suction lift also suffers and adjustments must be made. The table below illustrates the equivalent suction lifts for various alitudes. Example: At 6,000 feet elevation, a pump must be placed with 6.9 feet of the water to deliver as much water in GPM (gallons per minute) as the same unit would at a 10 -foot suction lift at sea level.

| Elevation | Suction Lifts (in Feet) |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Sea Level | 10.0 | 15.0 | 20.0 | 25.0 |
| 2,000 Feet | 8.8 | 13.2 | 17.6 | 22.0 |
| 4,000 Feet | 7.8 | 11.7 | 15.6 | 19.5 |
| 6,000 Feet | 6.9 | 10.4 | 13.8 | 17.3 |
| 8,000 Feet | 6.2 | 9.3 | 12.4 | 15.5 |
| 10,000 Feet | 5.7 | 8.6 | 11.4 | 14.3 |

NOTE: All references to GPM in this booklet refer to US gallons per minute.
(1) To convert imperial gallons to US gallons, multiply imperial gallons by 1.2.
(2) To convert US gallons to imperial gallons, multiply US gallons by 83 .

ENGINES, TOO, SUFFER FROM ALTITUDE

Most engines are rated by the manufacturer using 60 degrees Fahrenheit at sea level.

Deductions must be made from the rated horsepower as follows:

For each 1,000 feet above sea level, deduct $3.5 \%$, and $1 \%$ for each 10 degrees Fahrenheit above 60 degrees.

# Friction Loss Through 100' of Hose or Pipe 

Loss is given in feet of head. Based on Williams \& Hazen formula using constant 100. Sizes of standard pipe in inches.


## Friction Loss in Pipe Fittings

(EXPRESSED AS EQUIVALENT LENGTHS OF STRAIGHT PIPE)

| Nom <br> Pipe Dia. | VALVES - FULL OPEN |  |  |  |  |  |  | ELLS |  |  |  |  |  |  | TEES |  | ENLGMT |  | CONTRN |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | GATE | PLUG | $\begin{gathered} \text { GLOB } \\ \mathrm{E} \end{gathered}$ | $\begin{gathered} \text { ANGL } \\ \mathrm{E} \end{gathered}$ | $\begin{gathered} \text { SWG } \\ \text { CK } \end{gathered}$ | FOOT | $\begin{array}{\|c} \hline \text { SLUG } \\ \text { SHUT } \\ \text { OFF } \\ \hline \end{array}$ | $45^{\circ}$ | $90^{\circ}$ | $\begin{aligned} & L \quad R \\ & 90^{\circ} \end{aligned}$ | TUBE-TURN |  |  |  | STR THRU | $\begin{aligned} & \text { SIDE } \\ & \text { OUT'T } \end{aligned}$ | 1/2 | 3/4 | 1/2 | 3/4 |
|  |  |  |  |  |  |  |  |  |  |  | STD. |  | L. R. |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  | $45^{\circ}$ | $90^{\circ}$ | $45^{\circ}$ | $90^{\circ}$ |  |  |  |  |  |  |
| 11/2" | . 9 | - | 45 | 23 | 11 | 39 | 64 | 1.9 | 4.1 | 2.7 | 1.4 | 2.3 | 1.0 | 1.5 | 2.7 | 8.1 | 2.6 | 1.0 | 1.5 | 1.0 |
| 2" | 1.1 | 6.0 | 58 | 29 | 14 | 47 | 66 | 2.4 | 5.2 | 3.5 | 1.9 | 3.0 | 1.3 | 2.0 | 3.5 | 10.4 | 3.2 | 1.2 | 1.8 | 1.2 |
| 21/2" | 1.3 | 6.5 | 69 | 35 | 16 | 55 | 75 | 2.9 | 6.2 | 4.2 | 2.4 | 3.8 | 1.6 | 2.5 | 4.2 | 12.4 | 3.8 | 1.3 | 2.2 | 1.3 |
| 3" | 1.6 | 8 | 86 | 43 | 20 | 64 | 97 | 3.6 | 7.7 | 5.2 | 2.9 | 4.5 | 2.0 | 3.1 | 5.2 | 15.5 | 4.7 | 1.7 | 2.8 | 1.7 |
| 4" | 2.1 | 17 | 113 | 57 | 26 | 71 | 134 | 4.7 | 10.2 | 6.8 | 3.8 | 6.0 | 2.6 | 4.1 | 6.8 | 20.3 | 6.2 | 2.3 | 3.6 | 2.3 |
| 6" | 3.2 | 65 | 170 | 85 | 39 | 77 | 210 | 7.1 | 15.3 | 10.2 | 5.8 | 9.0 | 3.9 | 6.1 | 10.2 | 31 | 9.5 | 3.4 | 5.6 | 3.4 |
| 8" | 4.3 | 110 | - | 112 | 52 | 79 | 270 | 9.4 | 20.2 | 13.4 | 7.7 | 12 | 5.2 | 8.1 | 13.4 | 40 | 13 | 4.5 | 7.4 | 4.5 |
| 10" | 5.3 | 150 | - | 141 | 65 | 81 | 330 | 11.8 | 25.3 | 17 | 9.6 | 15 | 6.5 | 10.2 | 16.9 | 51 | 16 | 5.6 | 9.5 | 5.6 |
| 12" | 6.4 | - | - | 168 | 77 | 83 | 410 | 14.1 | 30 | 20 | 11.5 | 18 | 7.8 | 12.2 | 20.2 | 61 | 19 | 6.8 | 11 | 6.8 |

Friction Loss in Pounds Pressure
THROUGH ALUMNUM PIPE

| GPM | Pipe Size | Length of Pipe in Feet |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 100' | 200' | 500' | 1000' | 2000' | 3000' | 4000' | 5000' |
| 50 | $\begin{aligned} & \hline 2^{\prime \prime \prime} \\ & 3^{\prime \prime \prime} \\ & 4^{\prime \prime} \end{aligned}$ | $\begin{array}{r} 2.97 \\ .37 \\ .09 \end{array}$ | $\begin{aligned} & 6 . \\ & 0.74 \\ & 0.18 \\ & \hline \end{aligned}$ | $\begin{array}{r} 15 . \\ 2 . \\ 1 . \end{array}$ | $\begin{array}{r} 30 . \\ 4 . \\ 1 . \end{array}$ | $\begin{array}{r} 60 . \\ 8 . \\ 2 . \end{array}$ | $\begin{array}{r} 90 . \\ 12 . \\ 3 . \end{array}$ | $\begin{array}{r} 119 . \\ 15 . \\ 4 . \end{array}$ | $\begin{array}{r} 149 . \\ 19 . \\ 5 . \end{array}$ |
| 100 | $\begin{aligned} & \hline 2^{\prime \prime \prime} \\ & 3^{\prime \prime \prime} \\ & 4^{\prime \prime} \end{aligned}$ | $\begin{array}{r} 11.02 \\ 1.38 \\ .32 \end{array}$ | $\begin{gathered} 22 . \\ 3 . \\ 0.64 \end{gathered}$ | $\begin{array}{r} 56 . \\ 7 . \\ 2 . \\ \hline \end{array}$ | $\begin{array}{r} 111 . \\ 14 . \\ 4 . \end{array}$ | $\begin{array}{r} 221 . \\ 28 . \\ 7 . \end{array}$ | $\begin{aligned} & 42 . \\ & 10 . \end{aligned}$ | $\begin{aligned} & 56 . \\ & 13 . \end{aligned}$ | $\begin{aligned} & 69 . \\ & 16 . \end{aligned}$ |
| 150 | $\begin{aligned} & \hline 2^{\prime \prime \prime} \\ & 3^{\prime \prime \prime} \\ & 4^{\prime \prime} \end{aligned}$ | $\begin{array}{r} 20.13 \\ 2.82 \\ .69 \\ \hline \end{array}$ | $\begin{array}{r} 41 . \\ 6 . \\ 2 . \end{array}$ | $\begin{array}{r} 101 . \\ 15 . \\ 4 . \end{array}$ | $\begin{array}{r} 202 . \\ 29 . \\ 7 . \end{array}$ | $\begin{aligned} & 57 . \\ & 14 . \\ & \hline \end{aligned}$ | $\begin{aligned} & 85 . \\ & 21 . \\ & \hline \end{aligned}$ | $\begin{array}{r} 113 . \\ 28 . \\ \hline \end{array}$ | $\begin{array}{r} 141 . \\ 35 . \\ \hline \end{array}$ |
| 200 | $\begin{aligned} & 3^{\prime \prime} \\ & 4^{\prime \prime \prime} \\ & 6^{\prime \prime} \end{aligned}$ | $\begin{array}{r} 5.13 \\ 1.21 \\ .16 \end{array}$ | $\begin{gathered} 11 . \\ 3 . \\ 0.32 \end{gathered}$ | $\begin{array}{r} 26 . \\ 7 . \\ 1 . \end{array}$ | $\begin{array}{r} 52 . \\ 13 . \\ 2 . \\ \hline \end{array}$ | $\begin{array}{r} 103 . \\ 25 . \\ 4 . \end{array}$ | $\begin{array}{r} 154 . \\ 37 . \\ 5 . \end{array}$ | $\begin{array}{r} 206 . \\ 49 . \\ 7 . \end{array}$ | $\begin{array}{r} 257 . \\ 61 . \\ 8 . \end{array}$ |
| 300 | $\begin{aligned} & \hline 3^{\prime \prime} \\ & 4^{\prime \prime \prime} \\ & 6^{\prime \prime} \end{aligned}$ | $\begin{array}{r} 11.05 \\ 2.60 \\ .34 \end{array}$ | $\begin{aligned} & 22 . \\ & 6 . \\ & 0.68 \end{aligned}$ | $\begin{array}{r} 56 . \\ 13 . \\ 2 . \end{array}$ | $\begin{array}{r} 111 . \\ 26 . \\ 4 . \end{array}$ | $\begin{array}{r} 221 . \\ 52 . \\ 7 . \end{array}$ | $\begin{array}{r} 332 . \\ 78 . \\ 11 . \end{array}$ | $\begin{array}{r} 104 . \\ 14 . \end{array}$ | $\begin{array}{r} 130 . \\ 17 . \end{array}$ |
| 400 | $\begin{aligned} & \hline 4^{\prime \prime} \\ & 6^{\prime \prime \prime} \\ & 8^{\prime \prime} \end{aligned}$ | $\begin{array}{r} 4.50 \\ .59 \\ .14 \end{array}$ | $\begin{aligned} & 9 . \\ & 1 . \\ & 0.28 \end{aligned}$ | $\begin{array}{r} 23 . \\ 3 . \\ 1 . \end{array}$ | $\begin{array}{r} 23 . \\ 3 . \\ 1 . \end{array}$ | $\begin{array}{r} 90 . \\ 12 . \\ 3 . \end{array}$ | $\begin{array}{r} 135 . \\ 18 . \\ 5 . \end{array}$ | $\begin{array}{r} 180 . \\ 24 . \\ 6 . \end{array}$ | $\begin{array}{r} 225 . \\ 30 . \\ 7 . \end{array}$ |
| 500 | $\begin{aligned} & 4^{\prime \prime \prime} \\ & 6^{\prime \prime \prime} \\ & 8^{\prime \prime} \end{aligned}$ | $\begin{array}{r} \hline 6.83 \\ .89 \\ .22 \\ \hline \end{array}$ | 14. 2. 0.44 | $\begin{array}{r} 35 . \\ 5 . \\ 2 . \end{array}$ | $\begin{array}{r} 35 . \\ 5 . \\ 2 . \end{array}$ | $\begin{array}{r} 137 . \\ 18 . \\ 5 . \end{array}$ | $\begin{array}{r} 205 . \\ 27 . \\ 7 . \end{array}$ | $\begin{array}{r} 274 . \\ 36 . \\ 9 . \end{array}$ | $\begin{array}{r} \hline 342 . \\ 45 . \\ 11 . \end{array}$ |
| 600 | $\begin{aligned} & \hline 4^{\prime \prime \prime} \\ & 6^{\prime \prime \prime} \\ & 8^{\prime \prime} \end{aligned}$ | $\begin{array}{r} 9.75 \\ 1.28 \\ .31 \end{array}$ | $\begin{gathered} 20 . \\ 3 . \\ 0.62 \end{gathered}$ | $\begin{array}{r} 49 . \\ 7 . \\ 2 . \end{array}$ | $\begin{array}{r} 49 . \\ 7 . \\ 2 . \end{array}$ | $\begin{array}{r} 195 . \\ 26 . \\ 7 . \end{array}$ | $\begin{array}{r} 293 . \\ 39 . \\ 10 . \end{array}$ | $\begin{aligned} & 52 . \\ & 13 . \end{aligned}$ | $\begin{aligned} & 64 . \\ & 16 . \\ & \hline \end{aligned}$ |
| 700 | $\begin{aligned} & 6^{\prime \prime} \\ & 8^{\prime \prime} \end{aligned}$ | $\begin{array}{r} 1.70 \\ .42 \end{array}$ | 4. 1. | 9. 3. | $\begin{aligned} & 9 . \\ & 3 . \end{aligned}$ | $34 .$ $9 .$ | $\begin{aligned} & 51 . \\ & 13 . \end{aligned}$ | $\begin{aligned} & 68 . \\ & 17 . \end{aligned}$ | $\begin{aligned} & 85 . \\ & 21 . \end{aligned}$ |
| 800 | 6" 8 | $\begin{array}{r} 2.18 \\ \hline .54 \\ \hline \end{array}$ | 5. 1. | 11. | $\begin{array}{r} 11 . \\ 3 . \end{array}$ | $\begin{aligned} & 44 . \\ & 11 . \end{aligned}$ | $\begin{aligned} & 66 . \\ & 17 . \end{aligned}$ | $\begin{aligned} & 88 . \\ & 22 . \end{aligned}$ | $\begin{array}{r} 109 . \\ 27 . \end{array}$ |
| 1000 | 6" $8 \prime$ | $\begin{array}{r} 3.35 \\ .82 \\ \hline \end{array}$ | 7. | $\begin{array}{r} 17 . \\ 5 . \end{array}$ | $\begin{array}{r} 17 . \\ 5 . \end{array}$ | 67. 17. | $\begin{array}{r} 101 . \\ 25 . \end{array}$ | $\begin{array}{r} 134 . \\ 33 . \end{array}$ | $\begin{array}{r} 168 . \\ 41 . \end{array}$ |
| 1200 | $\begin{aligned} & 6^{\prime \prime \prime} \\ & 8^{\prime \prime} \end{aligned}$ | $\begin{aligned} & 4.72 \\ & 1.16 \end{aligned}$ | $\begin{array}{r} 10 . \\ 3 . \end{array}$ | $\begin{array}{r} 24 . \\ 6 . \\ \hline \end{array}$ | $\begin{array}{r} 24 . \\ 6 . \end{array}$ | $\begin{aligned} & 95 . \\ & 24 . \end{aligned}$ | $\begin{array}{r} 142 . \\ 35 . \end{array}$ | $\begin{array}{r} 189 . \\ 47 \end{array}$ | $\begin{array}{r} 236 . \\ 58 . \end{array}$ |
| 1400 | $\begin{aligned} & \hline 6^{\prime \prime} \\ & 8^{\prime \prime} \end{aligned}$ | $\begin{aligned} & 6.36 \\ & 1.56 \end{aligned}$ | $\begin{array}{r} 13 . \\ 3 . \end{array}$ | $\begin{array}{r} 32 . \\ 8 . \end{array}$ | $\begin{array}{r} 32 . \\ 8 . \end{array}$ | $\begin{array}{r} 128 . \\ 32 . \end{array}$ | $\begin{array}{r} 191 . \\ 47 . \end{array}$ | $\begin{array}{r} 255 . \\ 63 . \end{array}$ | $\begin{array}{r} 318 . \\ 78 . \end{array}$ |

## To Convert

| $\begin{gathered} \hline \text { POUNDS PRESSURE } \\ \text { TO } \\ \text { FEET OF HEAD } \end{gathered}$ |  | FEET OF HEADTOPOUNDS PRESSURE |  |
| :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { POUNDS } \\ \text { PRESSURE (PSI) } \end{gathered}$ | $\begin{aligned} & \text { FEET } \\ & \text { HEAD } \end{aligned}$ | $\begin{aligned} & \hline \text { FEET } \\ & \text { HEAD } \end{aligned}$ | POUNDS PRESSURE (PSI) |
| 1 | 2.31 | 1 | 0.43 |
| 2 | 4.62 | 2 | 0.87 |
| 3 | 6.93 | 3 | 1.30 |
| 4 | 9.24 | 4 | 1.73 |
| 5 | 11.55 | 5 | 2.17 |
| 6 | 13.85 | 6 | 2.60 |
| 7 | 16.16 | 7 | 3.03 |
| 8 | 18.47 | 8 | 3.46 |
| 9 | 20.78 | 9 | 3.90 |
| 10 | 23.09 | 10 | 4.33 |
| 20 | 46.18 | 20 | 8.66 |
| 30 | 69.27 | 30 | 12.99 |
| 40 | 92.36 | 40 | 17.32 |
| 50 | 115.49 | 50 | 21.65 |
| 60 | 138.54 | 60 | 25.99 |
| 70 | 161.63 | 70 | 30.32 |
| 80 | 184.72 | 80 | 34.65 |
| 90 | 207.80 | 90 | 38.98 |
| 100 | 230.90 | 100 | 43.31 |
| 120 | 277.07 | 120 | 51.97 |
| 140 | 323.25 | 140 | 60.63 |
| 160 | 369.43 | 160 | 69.29 |
| 180 | 415.61 | 180 | 77.96 |
| 200 | 461.78 | 200 | 86.62 |
| 300 | 692.69 | 300 | 129.93 |
| 400 | 922.58 | 400 | 173.24 |
| 500 | 1154.48 | 500 | 216.55 |

## Capacity and Flow Chart

Table One
Amount of water per foot in excavations

Table Two

Approximate flow of streams in U.S. Gallons per minute (Stream flow rate: 1' per second)

| Diameter <br> of Pool <br> of Water | U.S. Gallons <br> per Foot <br> of Depth |
| :---: | :---: |
| $1^{\prime}$ | 6 |
| $2^{\prime}$ | 24 |
| $3^{\prime}$ | 53 |
| $4^{\prime}$ | 94 |
| $5^{\prime}$ | 147 |
| $6^{\prime}$ | 212 |
| $77^{\prime}$ | 288 |
| $8^{\prime}$ | 376 |
| $9^{\prime}$ | 476 |
| $10^{\prime}$ | 587 |
| $15^{\prime}$ | 1320 |
| $20^{\prime}$ | 2350 |
| $25^{\prime}$ | 3672 |
| $30^{\prime}$ | 5275 |
| $35^{\prime}$ | 7200 |
| $40^{\prime}$ | 9500 |
| $45^{\prime}$ | 11900 |
| $50^{\prime}$ | 14700 |


| Depth of Stream at Midpoint | Width of Stream in Feet |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 3 | 5 | 10 |
| $1 "$ | 14 | 43 | 72 | 144 |
| 2" | 39 | 121 | 202 | 404 |
| $3 "$ | 71 | 221 | 370 | 740 |
| 4" | 108 | 338 | 569 | 1139 |
| 5" | 148 | 470 | 794 | 1588 |
| $6 "$ | 190 | 614 | 1040 | 2080 |
| $7{ }^{\prime \prime}$ | 244 | 771 | 1304 | 2608 |
| 8" |  | 935 | 1582 | 3164 |
| $9 "$ |  | 1106 | 1879 | 3759 |
| 10 " |  | 1286 | 2196 | 4392 |
| $11^{\prime \prime}$ |  | 1486 | 2542 | 5084 |
| 12 " |  | 1674 | 2866 | 5732 |
| 13 " |  | 1864 | 3204 | 6408 |
| $14 "$ |  | 2086 | 3592 | 7184 |
| 15" |  | 2296 | 3968 | 7936 |
| $16^{\prime \prime}$ |  | 2516 | 4360 | 8720 |
| $17^{\prime \prime}$ |  | 2770 | 4788 | 9576 |
| $18{ }^{\prime \prime}$ |  | 2964 | 5160 | 10320 |
| 19" |  | 3192 | 5576 | 11152 |

To estimate large areas of water, remember:
$71 / 2$ gallons = 1 cubic foot ( $\left.1^{\prime} \times 1^{\prime} \times 1^{\prime}\right)$
Example: Assume we have an area $500^{\prime}$ by $750^{\prime}$ covered with water to a depth of 3'
$500 \times 750 \times 3=1,125,000$ cubic feet
$1,125,000 \times 7.50-8,437,500$ gallons to be removed

If the water were to be removed at a rate of 1000 GPM , it would take 140 hours of continuous pumping to do the job.

From this, you can see it pays to take the time to estimate the amount of water to be pumped.

## Theoretical Discharge of Nozzles

## IN U.S. GALLONS PER MINUTE

| HEAD |  | Velocity of Discharge in Feet per Second | DIAMETER OF NOZZLES IN INCHES |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pounds | Feet |  | 1/16 | 1/8 | 3/16 | 1/4 | 3/8 | 1/2 | 5/8 | 3/4 | 7/8 |
| $\begin{aligned} & 10 \\ & 15 \\ & 20 \\ & 25 \\ & 30 \end{aligned}$ | $\begin{aligned} & 23.1 \\ & 34.6 \\ & 462 \\ & 57.7 \\ & 69.3 \end{aligned}$ | $\begin{gathered} 38.6 \\ 47.25 \\ 54.55 \\ 61.0 \\ 68.85 \end{gathered}$ | $\begin{aligned} & 0.37 \\ & 0.45 \\ & 0.52 \\ & 0.58 \\ & 0.64 \end{aligned}$ | $\begin{aligned} & 1.48 \\ & 1.81 \\ & 2.09 \\ & 2.34 \\ & 2.56 \end{aligned}$ | $\begin{aligned} & 3.32 \\ & 4.06 \\ & 4.69 \\ & 5.25 \\ & 5.75 \end{aligned}$ | $\begin{aligned} & 5.91 \\ & 7.24 \\ & 8.35 \\ & 9.34 \\ & 10.2 \end{aligned}$ | $\begin{aligned} & 13.3 \\ & 16.3 \\ & 18.8 \\ & 21.0 \\ & 23.0 \end{aligned}$ | $\begin{aligned} & 23.6 \\ & 28.9 \\ & 33.4 \\ & 37.3 \\ & 40.9 \end{aligned}$ | $\begin{aligned} & 36.9 \\ & 45.2 \\ & 52.2 \\ & 58.3 \\ & 63.9 \end{aligned}$ | $\begin{aligned} & 53.1 \\ & 65.0 \\ & 75.1 \\ & 84.0 \\ & 92.0 \end{aligned}$ | $\begin{aligned} & 72.4 \\ & 88.5 \\ & 102 \\ & 114 \\ & 125 \end{aligned}$ |
| $\begin{aligned} & 35 \\ & 40 \\ & 45 \\ & 50 \\ & 55 \\ & \hline \end{aligned}$ | $\begin{array}{r} 80.8 \\ 92.3 \\ 103.9 \\ 115.5 \\ 127.0 \\ \hline \end{array}$ | $\begin{gathered} 72.2 \\ 77.2 \\ 81.8 \\ 86.25 \\ 90.4 \\ \hline \end{gathered}$ | $\begin{aligned} & 0.69 \\ & 0.74 \\ & 0.78 \\ & 0.83 \\ & 0.87 \end{aligned}$ | $\begin{aligned} & 2.77 \\ & 2.96 \\ & 3.13 \\ & 3.30 \\ & 3.46 \\ & \hline \end{aligned}$ | $\begin{aligned} & 6.21 \\ & 6.64 \\ & 7.03 \\ & 7.41 \\ & 7.77 \end{aligned}$ | $\begin{aligned} & 11.1 \\ & 11.8 \\ & 12.5 \\ & 13.2 \\ & 13.8 \\ & \hline \end{aligned}$ | $\begin{aligned} & 24.8 \\ & 26.6 \\ & 28.2 \\ & 29.7 \\ & 31.1 \end{aligned}$ | $\begin{aligned} & 44.2 \\ & 47.3 \\ & 50.1 \\ & 52.8 \\ & 55.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 69.0 \\ & 73.8 \\ & 78.2 \\ & 82.5 \\ & 86.4 \end{aligned}$ | $\begin{gathered} \hline 99.5 \\ 106 \\ 113 \\ 119 \\ 125 \\ \hline \end{gathered}$ | $\begin{aligned} & 135 \\ & 145 \\ & 153 \\ & 162 \\ & 169 \end{aligned}$ |
| $\begin{aligned} & 60 \\ & 65 \\ & 70 \\ & 75 \\ & 80 \end{aligned}$ | $\begin{aligned} & 138.6 \\ & 150.1 \\ & 161.7 \\ & 173.2 \\ & 184.8 \end{aligned}$ | $\begin{gathered} 94.5 \\ 98.3 \\ 102.1 \\ 105.7 \\ 109.1 \end{gathered}$ | $\begin{aligned} & 0.90 \\ & 0.94 \\ & 0.98 \\ & 1.01 \\ & 1.05 \end{aligned}$ | $\begin{aligned} & 3.62 \\ & 3.77 \\ & 3.91 \\ & 4.05 \\ & 4.18 \end{aligned}$ | $\begin{aligned} & 8.12 \\ & 8.45 \\ & 8.78 \\ & 9.09 \\ & 9.39 \end{aligned}$ | $\begin{aligned} & 14.5 \\ & 15.1 \\ & 15.7 \\ & 16.2 \\ & 16.7 \end{aligned}$ | $\begin{aligned} & 32.5 \\ & 33.8 \\ & 35.2 \\ & 36.4 \\ & 37.6 \end{aligned}$ | $\begin{aligned} & 57.8 \\ & 60.2 \\ & 62.5 \\ & 64.7 \\ & 66.8 \end{aligned}$ | $\begin{aligned} & 90.4 \\ & 94.0 \\ & 94.0 \\ & 97.7 \\ & 101 \\ & 104 \end{aligned}$ | $\begin{aligned} & 130 \\ & 136 \\ & 141 \\ & 146 \\ & 150 \end{aligned}$ | $\begin{aligned} & 177 \\ & 184 \\ & 191 \\ & 193 \\ & 205 \end{aligned}$ |
| $\begin{gathered} 85 \\ 90 \\ 95 \\ 100 \\ 105 \end{gathered}$ | $\begin{aligned} & 196.3 \\ & 207.9 \\ & 219.4 \\ & 230.9 \\ & 242.4 \end{aligned}$ | $\begin{aligned} & 112.5 \\ & 115.8 \\ & 119.0 \\ & 122.0 \\ & 125.0 \end{aligned}$ | $\begin{aligned} & 1.06 \\ & 1.11 \\ & 1.14 \\ & 1.17 \\ & 1.20 \end{aligned}$ | $\begin{aligned} & 4.31 \\ & 4.43 \\ & 4.56 \\ & 4.67 \\ & 4.79 \end{aligned}$ | $\begin{aligned} & 9.67 \\ & 9.95 \\ & 10.2 \\ & 10.5 \\ & 10.8 \end{aligned}$ | $\begin{aligned} & \hline 17.3 \\ & 17.7 \\ & 18.2 \\ & 18.7 \\ & 19.2 \end{aligned}$ | $\begin{aligned} & 38.8 \\ & 39.9 \\ & 41.0 \\ & 42.1 \\ & 43.1 \end{aligned}$ | $\begin{aligned} & \hline 68.9 \\ & 70.8 \\ & 72.8 \\ & 74.7 \\ & 76.5 \end{aligned}$ | $\begin{aligned} & 108 \\ & 111 \\ & 114 \\ & 117 \\ & 120 \end{aligned}$ | $\begin{aligned} & 155 \\ & 160 \\ & 164 \\ & 168 \\ & 172 \end{aligned}$ | $\begin{aligned} & 211 \\ & 217 \\ & 223 \\ & 229 \\ & 234 \end{aligned}$ |
| $\begin{aligned} & \hline 110 \\ & 115 \\ & 120 \\ & 125 \\ & 130 \end{aligned}$ | $\begin{aligned} & 254.0 \\ & 265.5 \\ & 277.1 \\ & 288.6 \\ & 300.2 \end{aligned}$ | $\begin{aligned} & 128.0 \\ & 130.9 \\ & 133.7 \\ & 136.4 \\ & 139.1 \end{aligned}$ | $\begin{aligned} & 1.23 \\ & 1.25 \\ & 1.28 \\ & 1.31 \\ & 1.33 \end{aligned}$ | $\begin{aligned} & 4.90 \\ & 5.01 \\ & 5.12 \\ & 5.22 \\ & 5.33 \end{aligned}$ | $\begin{aligned} & 11.0 \\ & 11.2 \\ & 11.5 \\ & 11.7 \\ & 12.0 \end{aligned}$ | $\begin{aligned} & \hline 19.6 \\ & 20.0 \\ & 20.5 \\ & 20.9 \\ & 21.3 \end{aligned}$ | $\begin{aligned} & 44.1 \\ & 45.1 \\ & 46.0 \\ & 47.0 \\ & 48.0 \end{aligned}$ | $\begin{aligned} & \hline 78.4 \\ & 80.1 \\ & 81.6 \\ & 83.5 \\ & 85.2 \end{aligned}$ | $\begin{aligned} & 122 \\ & 125 \\ & 128 \\ & 130 \\ & 133 \end{aligned}$ | $\begin{aligned} & 176 \\ & 180 \\ & 184 \\ & 188 \\ & 192 \end{aligned}$ | $\begin{aligned} & 240 \\ & 245 \\ & 251 \\ & 256 \\ & 261 \end{aligned}$ |
| $\begin{aligned} & 135 \\ & 140 \\ & 145 \\ & 150 \\ & 175 \\ & 200 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 311.7 \\ & 323.3 \\ & 334.8 \\ & 346.4 \\ & 404.1 \\ & 461.9 \\ & \hline \end{aligned}$ | $\begin{aligned} & 141.8 \\ & 144.3 \\ & 146.9 \\ & 149.5 \\ & 161.4 \\ & 172.6 \\ & \hline \end{aligned}$ | 1.36 1.38 1.41 1.43 1.55 1.65 | $\begin{aligned} & \hline 5.43 \\ & 5.53 \\ & 5.62 \\ & 5.72 \\ & 6.18 \\ & 6.61 \\ & \hline \end{aligned}$ | $\begin{aligned} & 12.2 \\ & 12.4 \\ & 12.6 \\ & 12.9 \\ & 13.9 \\ & 14.8 \\ & \hline \hline \end{aligned}$ | $\begin{aligned} & \hline 21.7 \\ & 22.1 \\ & 22.5 \\ & 22.9 \\ & 24.7 \\ & 26.4 \\ & \hline \end{aligned}$ | $\begin{aligned} & 48.9 \\ & 49.8 \\ & 50.6 \\ & 51.5 \\ & 55.6 \\ & 59.5 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 86.7 \\ & 88.4 \\ & 91.5 \\ & 98.8 \\ & 106 \end{aligned}$ | $\begin{aligned} & \hline 136 \\ & 138 \\ & 140 \\ & 143 \\ & 154 \\ & 165 \\ & \hline \end{aligned}$ | 195 199 202 206 222 238 | $\begin{aligned} & 266 \\ & 271 \\ & 275 \\ & 280 \\ & 302 \\ & 325 \\ & \hline \end{aligned}$ |
|  |  | Velocity of Discharge in Feet per Second | DIAMETER OF NOZZLES IN INCHES |  |  |  |  |  |  |  |  |
| Pounds | Feet |  | 1 | $11 / 3$ | $11 / 4$ | $13 / 8$ | $11 / 2$ | $13 / 4$ | 2 | $21 / 4$ | $21 / 2$ |
| $\begin{aligned} & 10 \\ & 15 \\ & 20 \\ & 25 \\ & 30 \\ & \hline \end{aligned}$ | $\begin{aligned} & 23.1 \\ & 34.6 \\ & 462 \\ & 57.7 \\ & 69.3 \end{aligned}$ | $\begin{gathered} 38.6 \\ 47.25 \\ 54.65 \\ 61.0 \\ 66.85 \end{gathered}$ | $\begin{gathered} 94.5 \\ 116.0 \\ 134 \\ 149 \\ 164 \end{gathered}$ | $\begin{aligned} & 120 \\ & 147 \\ & 169 \\ & 189 \\ & 207 \end{aligned}$ | $\begin{aligned} & 148 \\ & 181 \\ & 209 \\ & 234 \\ & 256 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 179 \\ & 219 \\ & 253 \\ & 283 \\ & 309 \end{aligned}$ | $\begin{aligned} & 213 \\ & 280 \\ & 301 \\ & 336 \\ & 368 \end{aligned}$ | $\begin{aligned} & 289 \\ & 354 \\ & 409 \\ & 458 \\ & 501 \end{aligned}$ | $\begin{aligned} & 378 \\ & 463 \\ & 535 \\ & 598 \\ & 655 \end{aligned}$ | $\begin{aligned} & 479 \\ & 585 \\ & 676 \\ & 756 \\ & 828 \\ & \hline \end{aligned}$ | $\begin{gathered} 591 \\ 723 \\ 835 \\ 934 \\ 1023 \\ \hline \end{gathered}$ |
| $\begin{aligned} & 35 \\ & 40 \\ & 45 \\ & 50 \\ & 55 \end{aligned}$ | $\begin{array}{r} 80.8 \\ 92.4 \\ 103.9 \\ 115.5 \\ 127.0 \end{array}$ | $\begin{gathered} 72.2 \\ 77.2 \\ 81.8 \\ 86.25 \\ 90.4 \end{gathered}$ | $\begin{aligned} & 177 \\ & 188 \\ & 200 \\ & 211 \\ & 221 \end{aligned}$ | $\begin{aligned} & 224 \\ & 239 \\ & 253 \\ & 267 \\ & 280 \end{aligned}$ | $\begin{aligned} & 277 \\ & 296 \\ & 313 \\ & 330 \\ & 346 \end{aligned}$ | $\begin{aligned} & 334 \\ & 357 \\ & 379 \\ & 399 \\ & 418 \end{aligned}$ | $\begin{aligned} & 398 \\ & 425 \\ & 451 \\ & 475 \\ & 498 \end{aligned}$ | $\begin{aligned} & 541 \\ & 578 \\ & 613 \\ & 647 \\ & 678 \end{aligned}$ | $\begin{aligned} & \hline 708 \\ & 756 \\ & 801 \\ & 845 \\ & 886 \end{aligned}$ | $\begin{gathered} 895 \\ 957 \\ 1015 \\ 1070 \\ 1121 \end{gathered}$ | $\begin{aligned} & 1106 \\ & 1182 \\ & 1252 \\ & 1320 \\ & 1385 \end{aligned}$ |
| $\begin{aligned} & 60 \\ & 65 \\ & 70 \\ & 75 \\ & 80 \end{aligned}$ | $\begin{aligned} & 138.6 \\ & 150.1 \\ & 161.7 \\ & 173.2 \\ & 184.8 \end{aligned}$ | $\begin{gathered} 94.5 \\ 98.3 \\ 102.1 \\ 105.7 \\ 109.1 \end{gathered}$ | $\begin{aligned} & 231 \\ & 241 \\ & 250 \\ & 259 \\ & 267 \end{aligned}$ | $\begin{aligned} & 293 \\ & 305 \\ & 317 \\ & 327 \\ & 338 \end{aligned}$ | $\begin{aligned} & 362 \\ & 376 \\ & 391 \\ & 404 \\ & 418 \end{aligned}$ | $\begin{aligned} & 438 \\ & 455 \\ & 473 \\ & 489 \\ & 505 \end{aligned}$ | $\begin{aligned} & 521 \\ & 542 \\ & 563 \\ & 582 \\ & 602 \end{aligned}$ | $\begin{aligned} & 708 \\ & 737 \\ & 765 \\ & 792 \\ & 818 \end{aligned}$ | $\begin{gathered} 926 \\ 964 \\ 1001 \\ 1037 \\ 1100 \end{gathered}$ | $\begin{aligned} & 1172 \\ & 1220 \\ & 1267 \\ & 1310 \\ & 1354 \end{aligned}$ | $\begin{aligned} & 1447 \\ & 1506 \\ & 1565 \\ & 1619 \\ & 1672 \end{aligned}$ |
| $\begin{gathered} \hline 85 \\ 90 \\ 95 \\ 100 \\ 105 \end{gathered}$ | $\begin{aligned} & 196.3 \\ & 207.9 \\ & 219.4 \\ & 230.9 \\ & 242.4 \end{aligned}$ | $\begin{aligned} & \hline 112.5 \\ & 115.8 \\ & 119.0 \\ & 122.0 \\ & 125.0 \end{aligned}$ | $\begin{aligned} & 276 \\ & 284 \\ & 292 \\ & 299 \\ & 306 \end{aligned}$ | $\begin{aligned} & 349 \\ & 359 \\ & 369 \\ & 378 \\ & 388 \end{aligned}$ | $\begin{aligned} & \hline 431 \\ & 443 \\ & 455 \\ & 467 \\ & 479 \end{aligned}$ | $\begin{aligned} & \hline 521 \\ & 536 \\ & 551 \\ & 565 \\ & 579 \end{aligned}$ | $\begin{aligned} & \hline 620 \\ & 638 \\ & 656 \\ & 672 \\ & 689 \end{aligned}$ | 844 868 892 915 937 | $\begin{aligned} & 1103 \\ & 1136 \\ & 1168 \\ & 1196 \\ & 1226 \end{aligned}$ | $\begin{aligned} & 1395 \\ & 1436 \\ & 1476 \\ & 1512 \\ & 1550 \end{aligned}$ | $\begin{aligned} & \hline 1723 \\ & 1773 \\ & 1824 \\ & 1870 \\ & 1916 \end{aligned}$ |
| $\begin{aligned} & \hline 110 \\ & 115 \\ & 120 \\ & 125 \\ & 130 \end{aligned}$ | $\begin{aligned} & 254.0 \\ & 265.5 \\ & 277.1 \\ & 288.6 \\ & 300.2 \end{aligned}$ | $\begin{aligned} & 128.0 \\ & 130.9 \\ & 133.7 \\ & 136.4 \\ & 139.1 \end{aligned}$ | $\begin{aligned} & 314 \\ & 320 \\ & 327 \\ & 334 \\ & 341 \end{aligned}$ | $\begin{aligned} & 397 \\ & 406 \\ & 414 \\ & 423 \\ & 432 \end{aligned}$ | $\begin{aligned} & 490 \\ & 501 \\ & 512 \\ & 522 \\ & 533 \end{aligned}$ | $\begin{aligned} & \hline 583 \\ & 606 \\ & 619 \\ & 632 \\ & 645 \end{aligned}$ | $\begin{aligned} & \hline 705 \\ & 720 \\ & 736 \\ & 751 \\ & 767 \end{aligned}$ | $\begin{gathered} \hline 960 \\ 980 \\ 1002 \\ 1022 \\ 1043 \end{gathered}$ | $\begin{aligned} & 1255 \\ & 1282 \\ & 1310 \\ & 1338 \\ & 1365 \end{aligned}$ | $\begin{aligned} & \hline 1588 \\ & 1621 \\ & 1659 \\ & 1690 \\ & 1726 \end{aligned}$ | $\begin{aligned} & 1961 \\ & 2005 \\ & 2050 \\ & 2090 \\ & 2132 \end{aligned}$ |
| $\begin{aligned} & 135 \\ & 140 \\ & 145 \\ & 150 \\ & 175 \\ & 200 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 311.7 \\ & 323.3 \\ & 334.8 \\ & 346.4 \\ & 404.1 \\ & 461.9 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 141.8 \\ & 144.3 \\ & 146.9 \\ & 149.5 \\ & 161.4 \\ & 172.6 \end{aligned}$ | $\begin{aligned} & 347 \\ & 354 \\ & 360 \\ & 366 \\ & 395 \\ & 423 \end{aligned}$ | $\begin{aligned} & \hline 439 \\ & 448 \\ & 455 \\ & 463 \\ & 500 \\ & 535 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 543 \\ & 553 \\ & 562 \\ & 572 \\ & 618 \\ & 660 \\ & \hline \end{aligned}$ | 565 663 680 692 747 799 | $\begin{aligned} & \hline 780 \\ & 795 \\ & 809 \\ & 824 \\ & 890 \\ & 950 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 1063 \\ & 1082 \\ & 1100 \\ & 1120 \\ & 1210 \\ & 1294 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 1390 \\ & 1415 \\ & 1440 \\ & 1466 \\ & 1582 \\ & 1691 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1759 \\ & 1790 \\ & 1820 \\ & 1853 \\ & 2000 \\ & 2140 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2173 \\ & 2212 \\ & 2250 \\ & 2290 \\ & 2473 \\ & 2645 \end{aligned}$ |

NOTE: The actual quantities will vary from these figures, the amount of variation depending upon the shape of the nozzle and the size of pipe at the point where the pressure is determined. With smooth taper nozzles, the actual discharge is about 94 percent of the figures given in the above tables.

## Where to Use Pumps

## CONSTRUCTION USES

■ Self-Priming Centrifugal Pumps<br>- General Purpose,<br>- High Pressure<br>■ Trash

## Pump Out -

1. Small excavations
(General Purpose \& Trash)
2. Foundations
(General Purpose \& Trash)
3. Manholes
(General Purpose \& Trash)
4. Several well points
(General Purpose)
5. Strip mines
(General Purpose)
6. Flood water
(General Purpose \& Trash)
7. Swimming Pools
(General Purpose)
8. Sewage by-passing
(Trash)
9. Jetting
(High Pressure)

Fill -

1. Water wagons
(General Purpose)
2. Swimming Pools
(General Purpose)

## General Uses -

1. Wash down equipment
(High Pressure)
2. Standby fire protection
(High Pressure)
3. Barge cleaning
(General Purpose \& Trash)
4. Marinas
(General Purpose, High Pressure \& Trash)

## CONSTRUCTION USES

## Diaphragm Pumps

1. Ditch \& manhole dewatering
2. Sewage by-passing
3. Small wellpoint systems
4. Septic tank cleaning
5. Any slow seepage requirement

## FARM USES

## Self-Priming Centrifugal Pumps <br> ■ General Purpose <br> - High Pressure <br> - Trash

## Irrigation Uses -

1. Truck farms
(General Purpose \& High Pressure)
2. Fill stock tanks
(General Purpose \& High Pressure)
3. Wash down barn areas
(High Pressure)
4. Transfer liquid manures
(Trash Pumps)
5. Washing of equipment
(High Pressure)
6. Pump out flood water
(General Purpose \& Trash)
7. Standby fire protection
(High Pressure)
8. Water transfer at fish farms
(General Purpose)
FARM USES

## ■ Diaphragm Pumps

1. Transfer liquified manures
2. Septic tank cleaning
3. Any slow seepage requirement
